# U.S. DEPARTMENT OF THE INTERIOR U.S. GEOLOGICAL SURVEY

LEVEL II BRIDGE SCOUR ANALYSIS FOR STRUCTURE 134026500200 ON ROUTE SC 265, CROSSING LITTLE FORK CREEK IN CHESTERFIELD COUNTY, SOUTH CAROLINA

By Noel M. Hurley, Jr. and Stephen T. Benedict

Prepared in cooperation with the SOUTH CAROLINA DEPARTMENT OF TRANSPORTATION



Columbia, South Carolina 1994

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#### **UNIT ABBREVIATIONS**

cubic foot per second	ft <sup>3</sup> /s
feet per second	ft/s
foot	ft
mile	mi
millimeter	mm
square foot	ft <sup>2</sup>
square mile	$mi^2$

#### OTHER ABBREVIATIONS

D/S
U/S
f/p
WSPRO
D <sub>50</sub>
SCDOT

In this report, the words "right" and "left" refer to directions that would be reported by an observer facing downstream.

Sea level: In this report, "sea level" refers to the National Geodetic Vertical Datum of 1929-- a geodetic datum derived from a general adjustment of the first-order level nets of the United States and Canada, formerly called Sea Level Datum of 1929.

#### Level II bridge scour analysis for structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina

by Noel M. Hurley, Jr. and Stephen T. Benedict

This report provides the results of the detailed Level II analysis of scour potential at structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina (figure 1 in pocket; figures 5-8). The site is located near the divide of the Piedmont and upper Coastal Plain physiographic provinces near the town of Jefferson in the western part of Chesterfield County. The drainage area for the site is 15.0 mi<sup>2</sup>, and is a predominantly rural drainage basin with little development in recent years. In the vicinity of the study site, the land is covered by moderate to dense woods consisting of hardwoods and pines.

In the study area, Little Fork Creek has a meandering channel with a slope of approximately 0.00496 ft/ft (26.2 ft/mi), an average channel top width of 32 ft and an average channel depth of 5.2 ft. The predominant channel bed material is sand ( $D_{50}$  is 0.93 mm) and the channel banks consist of a silty sand ( $D_{50}$  is 0.40 mm). In general, the banks have light to moderate woody vegetative cover and were noted to be relatively stable at the time of the Level I and Level II site visits, March 31, 1992 and February 1 and 8, 1994, respectively.

The Route SC 265 crossing of Little Fork Creek is a 120-ft-long, two-lane bridge consisting of four 30-ft concrete spans, supported by concrete piers with spillthrough abutments. The left and right abutments have some riprap coverage but the riprap is in poor condition and the abutments have eroded. In this report, the words "right" and "left" refer to directions that would be reported by an observer facing downstream. Additional details describing conditions at the site are included in the Scour Report Summary.

Scour depths were computed using engineering judgement and the general guidelines described in Hydraulic Engineering Circular 18 (Richardson and others, 1993) and the Transportation Research Board Draft Paper, "Evaluating scour at bridges using WSPRO" (Arneson and others, 1992). Scour depths were calculated assuming an infinite depth of erosive material and a homogeneous particle-size distribution. The results of the scour analysis are presented in tables 1 through 5 and graphs of the scour depths are shown on figures 2 and 3.

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	penetration dep road plan boring the scour depths	oridge plans were a ths were determin gs (file number 43 s shown in this stu- the back of the repo	ed. In additio 5) show subsu dy. For more i	n, it should l rface rock and	oe noted that the d gravel that co	ne SCDOT ould affect
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Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina

Remaining pile/footing penetration (feet)			ţ	1		1	ŀ	i
Elevation of scour, USGS datum (feet)			-2.3	-2.8		-6.5	4.2	4.7
Total <sup>4</sup> scour depth (feet)	r second	5.7	7.6	7.6	r second	6.2	5.6	9.5
Ground elevation at pier/bent, USGS datum (feet)	100-year discharge is 1,740 cubic feet per second	-0.3	5.3	4.8	500-year discharge is 2,310 cubic feet per second	-0.3	5.3	4.8
Pile tip/ footing elevation, USGS datum (feet)	discharge is 1,7	1	I	ı	discharge is 2,3	1	ţ	ı*
Pile tip/ footing elevation, SCDOT datum (feet)	100-year	£.	1	-	500-year	1	l	4
Station from left end of bridge (feet)		30	09	96		30	09	06
Pier/bent <sup>1</sup> number		4	е	2		4	8	2

<sup>&</sup>lt;sup>1</sup> Pier/bent number corresponds to South Carolina Department of Transportation (SCDOT) road plans.

NOTE: The SCDOT road plan borings (file number 435) show subsurface rock and gravel that could reduce the scour depths shown in the above table. For more information, see the SCDOT plans in report pocket.

<sup>&</sup>lt;sup>2</sup> Stations are determined from left to right looking downstream.

<sup>&</sup>lt;sup>3</sup> Dashes indicate no data. No as built pile tip/footing information was available from the SCDOT.

<sup>&</sup>lt;sup>4</sup> Total scour depth is the sum of the contraction and pier/bent scour depths.

 Table 2. --Remaining pile/footing penetration at piers/bents for the 100- and 500-year discharges at the downstream face of structure 134026500200

 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina

09		1	100-year discharge is 1,740 cubic feet per second  -3 0.4 5.7	scour depth (feet) second 5.7	USGS datum (feet) -5.3	pue/rooting penetration (feet)
	;	1	5.3	7.6	-2.3	r r
	500-year dis	scharge is 2,31	500-year discharge is 2,310 cubic feet per second	second	i	
	ŀ	1	0.4	6.2	-5.8	1
	ı	I	1.4	6.2	4.8	1
	1	‡	5.3	5.6	4.2	!

<sup>&</sup>lt;sup>1</sup> Pier/bent number corresponds to South Carolina Department of Transportation (SCDOT) road plans.

NOTE: The SCDOT road plan borings (file number 435) show subsurface rock and gravel that could reduce the scour depths shown in the above table. For more information, see the SCDOT plans in report pocket.

<sup>&</sup>lt;sup>2</sup> Stations are determined from left to right looking downstream.

<sup>&</sup>lt;sup>3</sup> Dashes indicate no data. No as built pile tip/footing information was available from the SCDOT.

<sup>&</sup>lt;sup>4</sup> Total scour depth is the sum of the contraction and pier/bent scour depths.

Table 3. -- Cumulative scour depths at piers/bents for the 100- and 500-year discharges at the upstream face of structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina

Pier/bent <sup>1</sup> number	Station from <sup>2</sup> left end of bridge (feet)	Contraction scour depth (feet)	Pier/bent scour depth without debris (feet)	Total <sup>3</sup> scour depth without debris (feet)
	100-year dischar	ge is 1,740 cubi	c feet per second	
4	30	$0.0^{4}$	5.7	5.7
3	60	1.9	5.7	7.6
2	90	1.9	5.7	7.6
	500-year dischar	ge is 2,310 cubi	c feet per second	
4	30	0.04	6.2	6.2
3	60	3.3	6.2	9.5
2	90	3.3	6.2	9.5

<sup>&</sup>lt;sup>1</sup> Pier/bent number corresponds to South Carolina Department of Transportation (SCDOT) bridge plans.

NOTE: The SCDOT road plan borings (file number 435) show subsurface rock and gravel that could reduce the scour depths shown in the above table. For more information, see the SCDOT plans in report pocket.

NOTE: The pier and contraction scour equations used in this scour analysis were those recommended in Hydraulic Engineering
Circular 18 (Richardson and others, 1993). Scour depths were calculated assuming an infinite depth of erosive material and a
homogeneous particle-size distribution.

<sup>&</sup>lt;sup>2</sup> Stations are determined from left to right looking downstream.

<sup>&</sup>lt;sup>3</sup> Total scour depth is the sum of the contraction and pier/bent scour depths.

<sup>&</sup>lt;sup>4</sup> The calculated contraction scour is a negative value, but was set equal to zero to reflect a more reasonable estimate of scour during peak flood conditions.

Table 4. --Cumulative scour depths at piers/bents for the 100- and 500-year discharges at the downstream face of structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina

Pier/bent <sup>1</sup> number	Station from <sup>2</sup> left end of bridge (feet)	Contraction scour depth (feet)	Pier/bent scour depth without debris (feet)	Total <sup>3</sup> scour depth without debris (feet)
	100-year dischar	rge is 1,740 cubic	c feet per second	1 <del>4 1 .</del> .
4	30	0.04	5.7	5.7
3	60	0.04	5.7	5.7
2	90	1.9	5.7	7.6
	500-year dischar	ge is 2,310 cubic	c feet per second	
4	30	0.04	6.2	6.2
3	60	$0.0^{4}$	6.2	6.2
2	90	3.3	6.2	9.5

<sup>&</sup>lt;sup>1</sup> Pier/bent number corresponds to South Carolina Department of Transportation (SCDOT) bridge plans.

NOTE: The SCDOT road plan borings (file number 435) show subsurface rock and gravel that could reduce the scour depths shown in the above table. For more information, see the SCDOT plans in report pocket.

NOTE: The pier and contraction scour equations used in this scour analysis were those recommended in Hydraulic Engineering Circular 18 (Richardson and others, 1993). Scour depths were calculated assuming an infinite depth of erosive material and a homogeneous particle-size distribution.

<sup>&</sup>lt;sup>2</sup> Stations are determined from left to right looking downstream.

<sup>&</sup>lt;sup>3</sup> Total scour depth is the sum of the contraction and pier/bent scour depths.

<sup>&</sup>lt;sup>4</sup> The calculated contraction scour is a negative value, but was set equal to zero to reflect a more reasonable estimate of scour during peak flood conditions.

Table 5. -- Abutment scour depths for the 100- and 500-year discharges at structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina

Recurrence interval for discharge	Discharge (cubic feet per second)	Depth of scour <sup>1, 2</sup> at left abutment (feet)	Depth of scour <sup>1, 2</sup> at right abutment (feet)
100-year	1,740	7.0	5.2
500-year	2,310	7.9	6.5

<sup>&</sup>lt;sup>1</sup> Abutment scour depths were calculated using the Froehlich (1989) live-bed abutment scour equation, assuming no abutment protection.

 $<sup>^2</sup>$  The words "right" and "left" refer to directions that would be reported by an observer facing downstream.

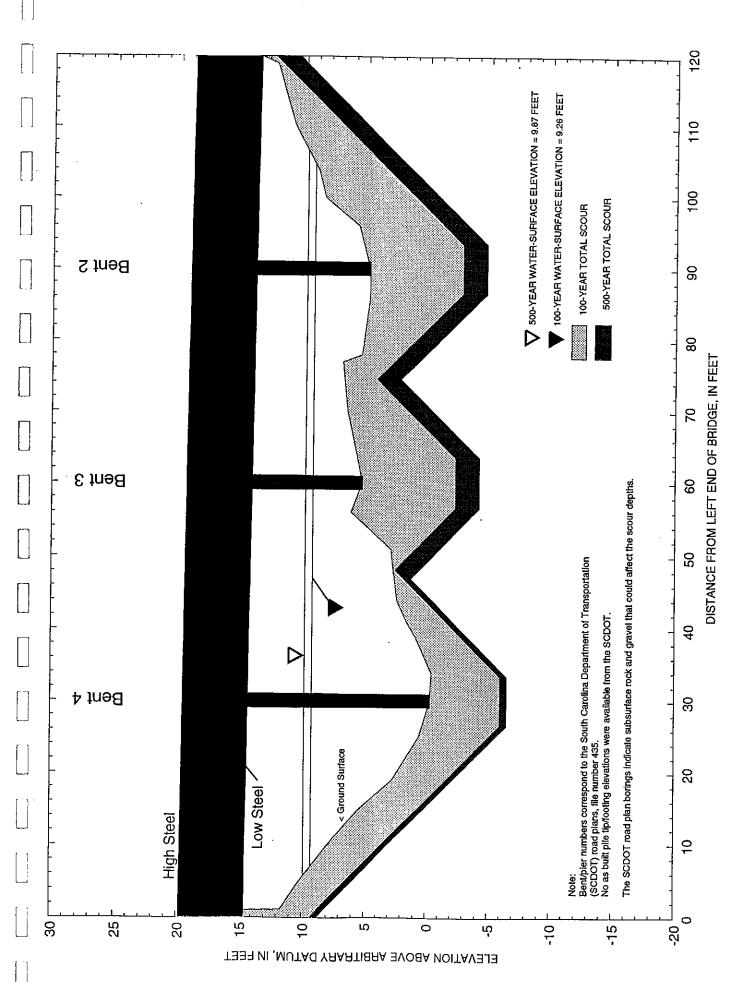


Figure 2.--Total scour depths for the 100- and 500-year discharges on the upstream face of structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina.

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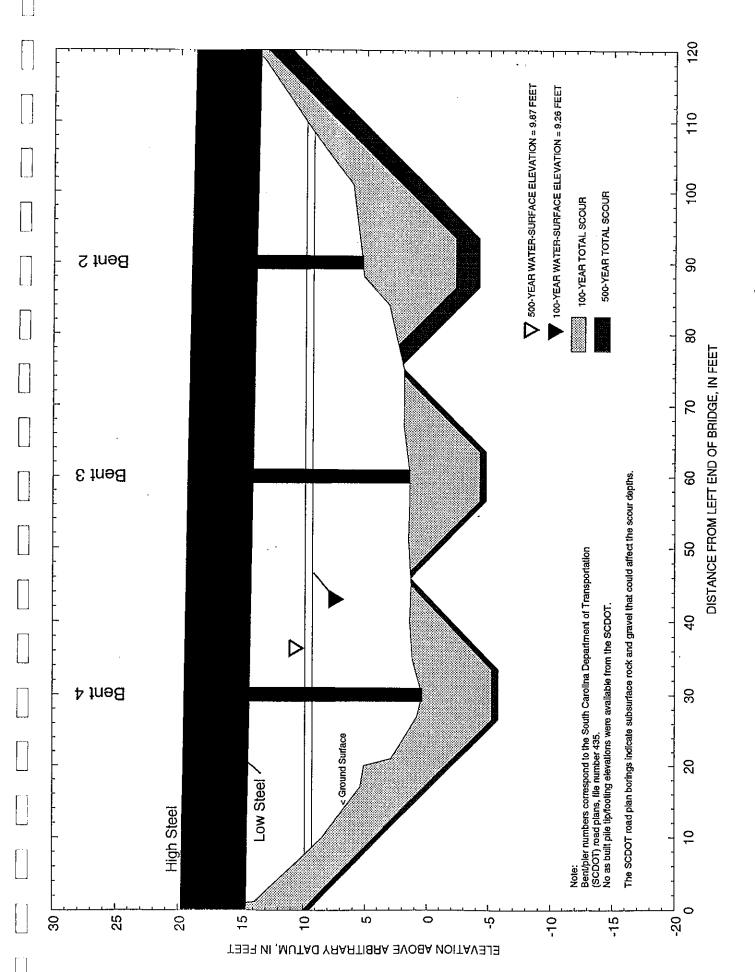


Figure 3.--Total scour depths for the 100- and 500-year discharges on the downstream face of structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina.

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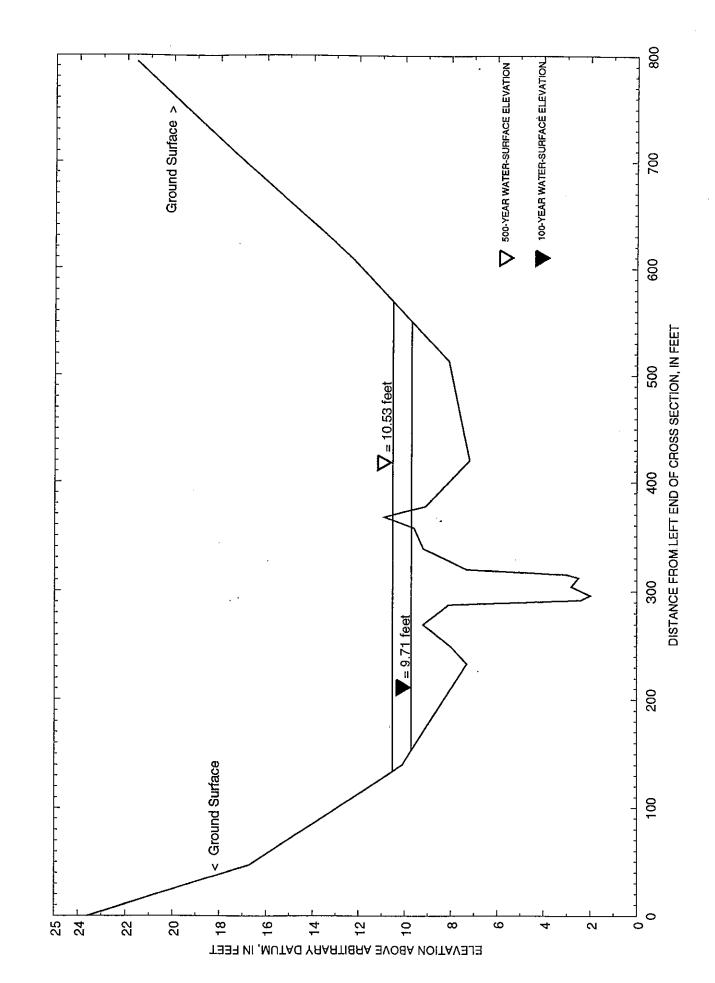


Figure 4.--Approach cross section of structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina.

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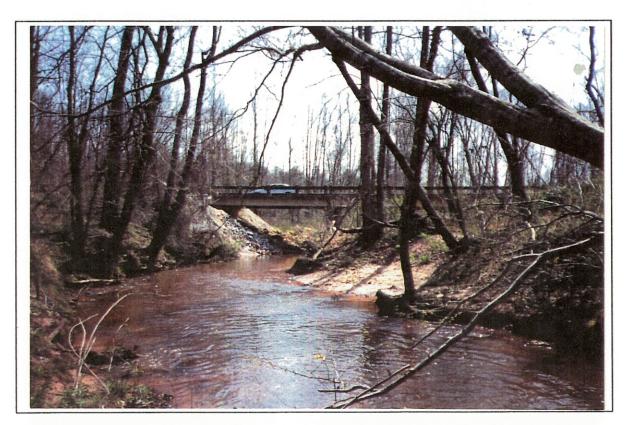
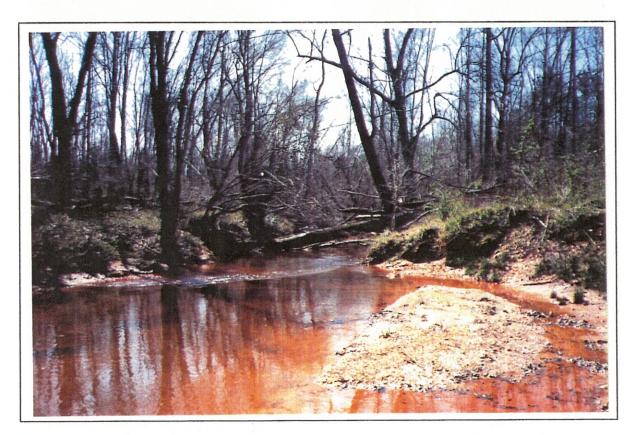
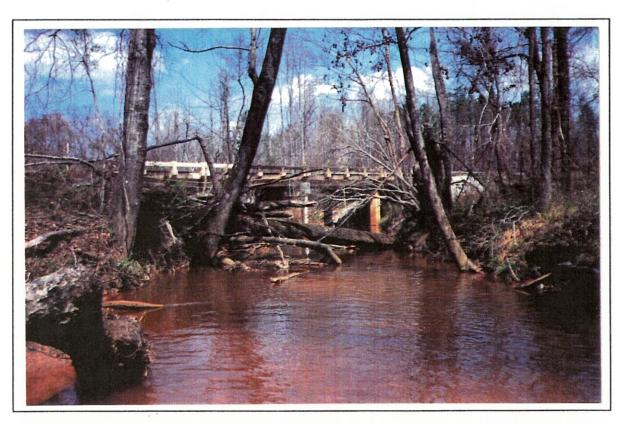


Figure 5.--Structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina as viewed from the upstream left bank (March 31, 1992).

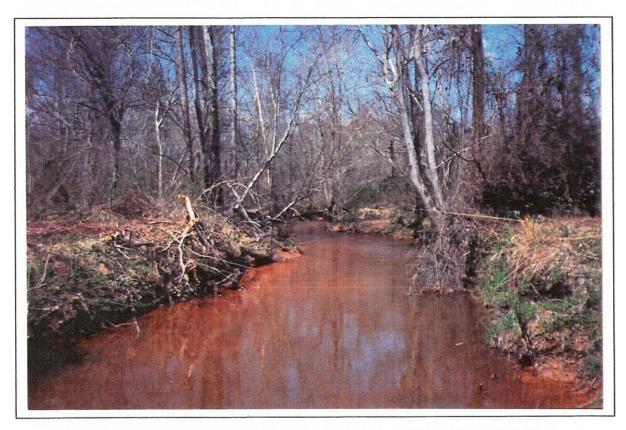


**Figure 6.**--Downstream channel as viewed from structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina (March 31, 1992).

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**Figure 7.-**-Structure 134026500200 on Route SC 265 crossing Little Fork Creek in Chesterfield, County, South Carolina, as viewed from the downstream channel (March 31, 1992).



**Figure 8.-**-Upstream channel as viewed from structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina (March 31, 1992).

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- Shearman, J. O., Kirby, W. H., Schneider, V. R., and Flippo, H. N., 1986, Bridge waterways analysis model; research report: Federal Highway Administration Publication FHWA-RD-86-108, 112 p.
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# SCOUR REPORT SUMMARY

cture Number     .	134026500200	Stream	Little Fo	rk Creek	
nty Chester	field	_ Road	SC 265	District	4
	<u>Descript</u>	ion of Brid	<u>ge</u>		
Bridge length _	120 ft Bridge wid	lth27	ft Max	x span length _	30 ft
	idge to road (on curve or				
Abutment type	Spillthrough	_ Embankm	ent type	Sloping	
	nent? Yes				
Description of	riprap The riprap on b	oth abutmen	ts is in poor	condition. The	2
bulkhead is exp	osed on the left abutmen	nt and the lov	ver half of th	ne right abutme	ent is
eroded.					
Is bridge locate The channel be upstream to 4 ft	d to flood plain according don a bend in channel? Independent to the right and flow downstream of the bridge at time of the of inspection	Yes If so, wimpacts the ge.	, describe (n left bank fro	nild, moderate, om approximat visit:	severe)
	Dute of inspection	blocked ho	rizontally		vertically
Level I	03-31-1992	45		2	0
Level II	02-01-1994				-
•	or debris Moderate: tre m of the bridge. Fallen			<del></del>	
• •	atures near or at the brid channel just downstream				ation date

# **Description of Flood Plain**

General top	ography The site is near the Fall line and has rolling hills and a narrow flood						
plain.							
Flood-plais	a conditions at bridge site: downstream (D/S), upstream (U/S)						
Date of ins	pection 02-08-1994						
D/S left:	Moderate hardwoods with moderate underbrush						
D/S right:	Moderate hardwoods with moderate underbrush and some pines on the edge of the f/p						
U/S left:	Light to moderate hardwoods with thick underbrush and briars						
U/S right:	Moderate hardwoods with moderate underbrush and briars						
	Description of Channel						
Average top	width 32 ft Average depth 5.2 ft						
Predomina	nt bed material Sand Bank material Silty sand						
Stream type	e (straight, meandering, braided, swampy, channelized) Meandering						
Vegetative o	cover on channel banks near bridge: Date of inspection 03-31-1992						
D/S left:	Light to moderate hardwood coverage						
D/S right:	Light to moderate hardwood coverage						
U/S left:	Light to moderate hardwood coverage						
U/S right:	Light to moderate hardwood coverage						
Do banks aj	opear stable? Yes If not, describe location and type of instability and						
date of obs	ervation. The banks are relatively stable with some areas of moderate to						
heavy fluv	ial erosion observed during the Level I site visit on March 31, 1992.						
	y obstructions in channel and date of observation. Fallen trees in channel						
just downs	tream of the bridge were observed on March 31, 1992.						
<del>-</del> .							

# <u>Hydrology</u>

Drainage area 15.0 mi <sup>2</sup>	
Percentage of drainage area in physiog	raphic provinces:
Physiographic province	Percent of drainage area
upper Coastal Plain	<u>47</u>
Piedmont	53
	<u> </u>
Is drainage area considered rural or urb	
urbanization and potential for develop	ment. The area has a low potential for
development.	
Is there a USGS gage on the stream of in	nterest? Yes
USGS gage descrip	Little Fork Creek near Jefferson, SC
USGS gage numbe	r 02131320
Gage drainage are	$a  15.0  mi^2$
Is there a lake/pond that will significan	tly affect hydrology/hydraulics?No
If so, describe	
et.	
-	
Calcul	lated Discharges
Q100 $1,740$ $ft^3/s$	$Q500 \ _{2,310} \ ft^3/s$
Method used to determine discharges	The discharges were estimated using the
methods described in WRIR 91-4157, "	Techniques for estimating magnitude and
frequency of floods in South Carolina,	1988", by W.B. Guimaraes and L.R. Bohman.
The data from gaging station 02131320	was not used because only for years of flow
data were available.	

# Brief Description of the Water-Surface Profile Model (WSPRO) Analysis Datum for WSPRO analysis (USGS survey, sea level, SCDOT plans) USGS survey Datum tie between USGS survey and SCDOT plans Add 65.9 ft to the USGS datum to obtain the SCDOT road plans' datum (file number 435). Description of reference marks used to determine USGS datum. RM 1 is the head of a lag bolt in a power pole on the right bank, 20 ft D/S of the bridge, elevation is 10.09 ft. RM 2 is a chiseled square on the D/S bridge rail, 10 ft left of the USGS gaging station, elevation is 18.98 ft. RM 3 is a steel bar on the U/S side of the bridge on the center span, elevation is 17.48 ft. Cross Sections Used in WSPRO Analysis

*Cross section ID	Section Reference Distance (SRD) in feet	**How cross section was developed	Comments
EXIT	-120	4	Exit cross section
FULV	. 0	4	Full-valley cross section
BRDGU	0	1	Upstream bridge face
APP	147	4	Approach cross section
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<sup>\*</sup> For location of cross sections see topographic map included with report (figure 1). For more detail on how cross sections were developed see WSPRO input file.

<sup>\*\*</sup> Cross section development: 1) survey at SRD 2) shift of survey data to SRD 3) modification of survey data based on topographic map 4) synthesized by combining channel survey data and SCDOT road plan data 5) other

#### Description of data and assumptions used in developing WSPRO model.

Little Fork Creek has a relatively uniform flood plain width in the study area, with no downstream natural or man-made contractions of flow that cause significant backwater at the Route SC 265 crossing. The flood plain begins to widen approximately 600 ft downstream of the bridge but was not included in the model because it is almost two flood-plain widths downstream of the Route SC 265 bridge. Therefore, it was assumed that slope-conveyance methodology would be adequate for estimating the starting-water-surface elevation for the water-surface profile computations.

For this study, the WSPRO model requires, as a minimum, an exit section one bridge width downstream of the bridge, a full-valley section at the downstream face of the bridge, the bridge section, and an approach section one bridge width upstream of the bridge. Cross sections at the upstream and downstream faces of the bridge were directly surveyed and the more constricted (upstream) bridge face was used in the WSPRO model. The section reference distance (SRD) at the downstream face of the bridge was set to zero. A Survey of the approach channel (located 122 ft upstream of the upstream bridge face) was adjusted by the channel slope and combined with the survey data from the SCDOT road plans (file number 435) for the Route SC 265 bridge. This cross section was shifted by the channel slope to the appropriate SRD to represent the exit, full-valley, and approach cross sections required by the WSPRO model.

#### **Bridge Hydraulics**

Average embankment elevation 16.6 ft

Average low steel elevation 14.3 ft

100-year discharge 1,740 ft<sup>3</sup>/s

Water-surface elevation at D/S bridge face 9.26 ft

Area of flow at D/S bridge face 441 ft<sup>2</sup>

Average velocity in bridge opening 3.95 ft/s

Maximum WSPRO tube velocity at bridge 5.54 ft/s

Water-surface elevation at Approach section with bridge 9.71 ft

Water-surface elevation at Approach section without bridge 9.59 ft

Amount of backwater caused by bridge 0.12 ft

500-year discharge \_\_\_2,310\_\_\_ ft<sup>3</sup>/s

Water-surface elevation at D/S bridge face \_\_\_\_9.87\_\_ ft

Area of flow at D/S bridge face \_\_\_\_498\_\_ ft<sup>2</sup>

Average velocity in bridge opening \_\_\_\_4.64\_\_ ft/s

Maximum WSPRO tube velocity at bridge \_\_\_\_6.54\_\_ ft/s

Water-surface elevation at Approach section with bridge 10.53 ft

Water-surface elevation at Approach section without bridge 10.29 ft

Amount of backwater caused by bridge 0.24 ft

#### **Scour**

Describe any special assumptions or considerations made in bridge scour analysis.

Scour depths were computed using engineering judgement and the general guidelines described in Hydraulic Engineering Circular 18 (Richardson and others, 1993) and the Transportation Research Board Draft Paper, "Evaluating scour at bridges using WSPRO" (Arneson and others, 1992). Scour depths were calculated assuming an infinite depth of erosive material and a homogeneous particle-size distribution. The results of the scour analysis are presented in tables 1 through 5 and graphs of the scour depths are shown on figures 2 and 3.

The local pier scour was determined using the Colorado State University pier scour equation (Richardson and others, 1993). Little Fork Creek expands significantly as it flows through the Route SC 265 bridge. The channel widens from 41 to 68 ft from the upstream to downstream bridge faces. This appears to be caused by high flows deflecting off the left bank just upstream of and at the bridge. Therefore, bents 2, 3, and 4 were analyzed as if they were in the channel to account for the possibility of additional channel widening and bank erosion occurring at the bridge during a flood. Ninety percent of the maximum WSPRO tube velocity and the maximum depth within the channel at the bridge were used to analyze the bents. The maximum depth within the channel was used to account for possible changes in the thalweg during a flood.

Figure 2, which represents the potential scour depths that could occur at the Route SC 265 crossing of Little Fork Creek, was developed using the more constricted (upstream) bridge face cross section. Because of the channel widening between the upstream and downstream bridge faces, figure 3 was included in the report to show the potential scour depths that could occur at the downstream face of the Route SC 265 bridge.

The right overbank at the bridge was analyzed for contraction scour using Laursen's clear-water contraction scour equation (Richardson and others, 1993). The left abutment is located on the left bank, therefore no left overbank scour computations were made. The channel contraction scour was analyzed using Laursen's modified live-bed contraction scour equation (Richardson and others, 1993).

The live-bed contraction scour equation indicates the deposition of sediment in the channel at the bridge during the 100- and 500-year floods. (See negative scour values determined in scour calculations included at the end of the report). However, it seems unreasonable to expect sediment deposition at the bridge during peak flood conditions. Therefore, the negative scour values were set equal to zero as reflected in tables 3 and 4 and figures 2 and 3.

The abutments are partially covered by riprap that is in poor condition and the abutments have eroded. Therefore, abutment scour was calculated using the Froehlich (1989) live-bed abutment scour equation.

It should be noted that the SCDOT road plan borings (file number 435) show subsurface rock and gravel that could affect the scour depths shown in this study. For more information, see the SCDOT bridge plans in the pocket at the back of the report.

#### WSPRO INPUT FILE

```
WSPRO PROFILES--STRUCTURE 134026500200
T1
T2
          LITTLE FORK CREEK AT ROUTE SC 265, CHESTERFIELD COUNTY, SC
Т3
          LEVEL II BRIDGE SCOUR ANALYSIS
J1
          * * * 0.85
                 Q500
*
           0100
           1740
0
                   2310
SK
           0.00496 0.00496
*
           THE TEMPLATE CROSS SECTION (TEMP) IS A COMBINATION OF THE SURVEY
           OF THE APPROACH CHANNEL AND GROUND POINTS TAKEN FROM SCDOT ROAD
*
           PLANS. THE APPROACH CHANNEL WAS SURVEYED 122 FT UPSTREAM OF THE
           BRIDGE. IN ADDITION, THE FLOOD-PLAIN DATA TAKEN FROM THE SCDOT
*
           ROAD PLANS WAS ADJUSTED FOR THE SKEW OF 20 DEGREES. THE CROSS
           SECTION WAS LOCATED AT THE APPROPRIATE SECTION REFERENCE DISTANCE
           AND THE DATA POINTS ADJUSTED BY THE CHANNEL SLOPE. THE DOWNSTREAM
           CHANNEL ROUGHNESS COEFFICIENTS WERE INCREASED SLIGHTLY TO ACCOUNT
           FOR LARGE DEBRIS IN THE CHANNEL.
XT
     TEMP
            149
            0 23.6 47 16.7 140 10.1 233
GR
                                              7.3 249 8.0
GR
            269
                9.2 287
                          8.1 292 2.4 296
                                              2.0 304 2.8-
GR
            312
                2.5 315
                          3.0 319 7.3 338
                                              9.2 357 9.6
GR
            368 10.9 378 9.1 420 7.2 513
                                              8.1 607 12.2
GR
            700 17.0 794 21.6
*
XS
    EXIT
           -120 * * * 0.00496
GΨ
            0.18 0.048 0.18
N
SA
                287 319
           0 * * * 0.00496
XS
    FULV
GT
*
           THE UPSTREAM BRIDGE FACE WAS THE MORE RESTRICTIVE AND WAS USED
           IN THE COMPUTATIONS. THE BRIDGE SKEW WAS DETERMINED FROM THE
           TOPOGRAPHIC MAP.
          SRD LOW STEEL SKEW
BR
    BRDGU 0 14.3
                        21
GR
            0 14.9
                    1 14.6 1.1 11.7 5 10.2 10 7.9
GR
               5.4 19 2.7 25
            15
                                 0.6 30 -0.3 34 -0.4
                        1.6 44
GR
           39
                0.9 41
                                   2.4 51
                                           3.0 56
                                                     6.2
                5.3 70
                         6.5 77
                                  6.9 78
           60
GR
                                          5.4 86
                                                    4.8
               4.8 96
GR
           90
                        5.7 100
                                 8.4 104
                                          9.0 110 10.9
GR
           119 12.4 120 13.7 0 14.9
N
           0.045 0.045 0.045
               15 56
SA
PW 1
          -0.3 1.9 4.8 1.9 4.8 3.8 5.3 3.8 5.3 5.7 14.3 5.7 14.3 0.0
CD
           3 27 1.6 16.6
```

#### WSPRO INPUT FILE -- Continued

```
THE APPROACH CROSS SECTION IS A COMBINATION OF THE SURVEY
            OF THE APPROACH CHANNEL AND GROUND POINTS TAKEN FROM SCDOT ROAD
                    THE APPROACH CHANNEL WAS SURVEYED 122 FT UPSTREAM OF THE
            BRIDGE AND THE APPROACH FLOOD PLAIN WAS TAKEN FROM THE ROAD PLANS
            THE CROSS SECTION WAS LOCATED AT THE APPROPRIATE SECTION REFERENCE
            DISTANCE AND THE DATA POINTS ADJUSTED BY THE CHANNEL SLOPE.
AS
     APP
            147 * * * 0.00496
GT
ВP
            272
Ν
            0.18
                    0.045
                              0.16 0.18
SA
                287
                         319
                               513
PΧ
              850
     EXIT
                    25
PΧ
     APP
              850
                    25
   BRDGU
PΧ
              120
                    25
HP 1 BRDGU
               9.26, ,9.26,1740
HP 2 BRDGU
               9.32, ,9.32,1740
HP 1 APP
               9.71, ,9.71,1740
HP 2 APP
               9.71, ,9.71,1740
HP 1 BRDGU
               9.87, ,9.87,2310
               9.94, ,9.94,2310
HP 2 BRDGU
              10.53, ,10.53,2310
HP 1 APP
              10.53, ,10.53,2310
HP 2 APP
*
EX
ER
```

### WSPRO OUTPUT

WSPRO	FEDERAL HIGHWAY	ADMINISTRATION WATER-SURFACE	- U. S. GEOLOGICA	L SURVEY			
V060188	MODEL FOR		PROFILE COMPUTAT	IONS			
WSPRO PROFILESSTRUCTURE 134026500200  LITTLE FORK CREEK AT ROUTE SC 265, CHESTERFIELD COUNTY, SC LEVEL II BRIDGE SCOUR ANALYSIS  *** RUN DATE & TIME: 10-05-94 11:07  CROSS-SECTION PROPERTIES: ISEQ = 3; SECID = BRDGU; SRD = 0.							
	1 14. 6 2 282. 338 3 145. 100	558. 7. 8 333. 38. 41 949. 46. 48	•	110. 4354. 1464			
WSEI	. LEW REW	J AREA	= BRDGU; SRD =  K Q VEL . 1740. 3.89	0.			
X STA.	6.9 19.3	22.2	24.5 26.5	28.4			
A(I)	36.3	19.2 17.7	16.7	16.1			
V(I)	2.40	4.54 4.90	5.21	5.39			
X STA.	28.4 30.2	32.0	33.7 35.6	37.5			
A(I)	15.7	15.9 16.0	16.8	15.9			
V(I)	5.54	5.46 5.42	5.19	5.47			
X STA.	37.5 39.5	42.0	44.9 48.0	51.5			
A(I)	16.2	17.9 19.0	19.5	20.9			
V(I)	5.38	4.86 4.57	4.47	4.17			
A(1)	36.4	30.6 33.1	82.0 88.4 26.3 3.31	40.5			

WSPRO V060188	FEDERAL MODE	HIGHWAY ADMI L FOR WATI	INISTRATION ER-SURFACE	- U. S. GEO PROFILE CO	DLOGICAL SUR	VEY
]	WSPRO PROFILE LITTLE FORK C LEVEL II BRID *** RUN DAT -SECTION PROP	REEK AT ROUT GE SCOUR ANA E & TIME: 10	TE SC 265, C ALYSIS )-05-94 11:	HESTERFIELI 07		
	SA# ARE. 1 172 2 207 3 294	A K . 1678 21726 3821.	TOPW WET 134. 134 32. 37 177. 178	P ALPH		QCR 1104. 2982.
Į.	TY DISTRIBUT: SEL LEW 0.71 152.6	REW A	AREA	K O	VEI.	<b>17</b> .
A(I)	152.6 135.7 0.64	7 61.1	. 11.3	10.7	11.1	
X STA. A(I) V(I)	296.7 11.0 7.88	11.0	11.5	11.4	302.8 11.5 7.58	
X STA. A(I) V(I)	304.5 11.5 7.54	306.1 5 11.6 1 7.48	307.8 11.5 7.59	309.4 11.3 7.73	311.0 11.3 7.67	312.5
A(I)	312.5 11.4 7.63	16.4	125.6	92.0	113.6	

		ADMINISTRATION - WATER-SURFACE P		
LEVE **	LE FORK CREEK AT L II BRIDGE SCOU * RUN DATE & TIM	CTURE 13402650020 ROUTE SC 265, CH R ANALYSIS E: 10-05-94 11:0 ISEQ = 3; SEC	ESTERFIELD COUNT	
WSEL SA	# AREA 1 19. 9' 2 306. 386: 3 173. 131:	K TOPW WETP 79. 9. 10. 21. 38. 41. 92. 47. 50.	ALPH LEW	REW QCR 159. 4905. 1877.
		92. 94. 100. SEQ = 3; SECID		
WSEL 9.94	LEW REW 5.6 107.0	AREA K 504.5 53785.	Q VEL 2310. 4.58	
X STA. A(I) V(I)	5.6 19.0 41.7 2.77	22.0 21.4 20.3 5.41 5.68	24.5 26.6 18.6 6.20	28.6 18.5 6.23
A(I)	18.1	32.4 17.7 18.5 6.54 6.23	18.5	18.6
A(I)	18.8	43.4 20.7 21.7 5.59 5.33	22.2	34.3
X STA. A(I) V(I)	30.8	74.9 36.2 33.2 3.19 3.48	28.4	46.4

WSPRO V060188				S. GEOLOGICA LE COMPUTAT	
LITTI LEVEI	PROFILESST LE FORK CREEK LII BRIDGE SC RUN DATE & T	AT ROUTE SC OUR ANALYSIS	265, CHESTER	RFIELD COUNTY	Y, SC
	ION PROPERTIE			APP ; SRD	= 147.
1 2 3 4	AREA 292. 233. 2 444. 68.	3704. 153. 5514. 32. 7294. 189. 645. 56.	153. 37. 189. 56.		REW QCR 2282. 3567. 3860. 428.
10.53	1037. 3	3156. 430.	435. 6.6	59 134. !	3530.
WSEL	DISTRIBUTION:  LEW RI  133.8 568	EW AREA	K	Q VEL	147.
X STA. 1 A(I) V(I)	.33.8 230 163.5 0.71	.2 290. 141.0 0.82	1 292.8 19.6 5.91	3 294.5 14.5 7.96	296.2 14.1 8.17
	14.3 8.10	14.2	14.5	15.1	14.8
	307 14.8 7.83	14.9	14.7	14.7	15.1
X STA. 3 A(I) V(I)	40.4	.3 416. 147.0 0.79	104.3	103.2	568.9 L41.8 0.81

	WSPRO FEDERAL HIGHWAY ADMINISTRATION - U. S. GEOLOGICAL SURVEY V060188 MODEL FOR WATER-SURFACE PROFILE COMPUTATIONS								
	WSPRO PROFILESSTRUCTURE 134026500200 LITTLE FORK CREEK AT ROUTE SC 265, CHESTERFIELD COUNTY, SC LEVEL II BRIDGE SCOUR ANALYSIS  *** RUN DATE & TIME: 10-05-94 11:07								
XSID:COI SI	DE SRDL RD FLEN	LEW REW	AREA K	VHD ALPH	HF HO	EGL ERR	CRWS FR#	Q VEL	WSEL
EXIT :XS -120	*****	155. 548.	671. 24704.	0.60 5.70	**** ****	8.90 ****	7.11 0.82	1740. 2.59	8.30
(	120. . 120. <<< <the< td=""><td>549.</td><td>24849.</td><td>5.73</td><td>0.00</td><td>0.01</td><td>0.81</td><td>2.57</td><td></td></the<>	549.	24849.	5.73	0.00	0.01	0.81	2.57	
147	147. . 147. <<< <the< td=""><td>547. ABOVE RES</td><td>26109. SULTS RE</td><td>5.54 FLECT</td><td>0.01 "NORMA</td><td>0.00 L" (UNCO</td><td>0.83 NSTRICTEI</td><td>2.64 D) FLOW&gt;&gt;</td><td></td></the<>	547. ABOVE RES	26109. SULTS RE	5.54 FLECT	0.01 "NORMA	0.00 L" (UNCO	0.83 NSTRICTEI	2.64 D) FLOW>>	
	<<< <r< td=""><td>ESULTS RI</td><td>EFLECTING</td><td>G THE</td><td>CONSTR</td><td>ICTED FL</td><td>OW FOLLOW</td><td>V&gt;&gt;&gt;&gt;</td><td></td></r<>	ESULTS RI	EFLECTING	G THE	CONSTR	ICTED FL	OW FOLLOW	V>>>>	
XSID:COI	DE SRDL LD FLEN	LEW REW	AREA K	VHD ALPH	HF HO	EGL ERR	CRWS FR#	Q VEL	WSEL
	120. 120.								9.26
	PPCD FLO 1. 1								
XSID:CO	DE SRDL RD FLEN	LEW REW	AREA K	VHD	HF HO	EGL ERR	CRWS FR#	Q VEL	WSEL
	120. 127.								9.71
	G) M(K) 55 0.191								

<><<END OF BRIDGE COMPUTATIONS>>>>

	WSPRO OUTPUTContinued									
	WSPRO V060188							GEOLOGICAI COMPUTAT:		
		WSPRO PRO LITTLE FOI LEVEL II I *** RUN	RK CREEK BRIDGE S	AT ROUT	E SC 2 LYSIS	265, CH	HESTERFIE	ELD COUNTY	ł, SC	
	XSID:CODI SRI	E SRDL D FLEN	LEW REW	AREA K	VHD ALPH	HF HO	EGL ERR	CRWS FR#	Q VEL	WSEL
	EXIT :XS -120	*****	137. 564.	949. 32781.	0.62 6.68	****	9.62 *****	7.97 0.74	2310. 2.43	9.00
		120. . 120. <<< <the a<="" th=""><th>565.</th><th>32959.</th><th>6.70</th><th>0.00</th><th>0.01</th><th>0.73</th><th>2.42</th><th></th></the>	565.	32959.	6.70	0.00	0.01	0.73	2.42	
	APP :AS	147. . 147. <<< <the a<="" th=""><th>137. 563. ABOVE RE</th><th>935. 34763. SULTS RE</th><th>0.62 6.51 FLECT</th><th>0.68 0.00 "NORMA</th><th>10.91 0.00 L" (UNCC</th><th>****** 0.74 NSTRICTEI</th><th>2310. 2.47 D) FLOW&gt;:</th><th>10.29</th></the>	137. 563. ABOVE RE	935. 34763. SULTS RE	0.62 6.51 FLECT	0.68 0.00 "NORMA	10.91 0.00 L" (UNCC	****** 0.74 NSTRICTEI	2310. 2.47 D) FLOW>:	10.29
Π		<<< <ri< th=""><th>ESULTS R</th><th>EFLECTIN</th><th>G THE</th><th>CONSTR</th><th>RICTED FI</th><th>OW FOLLOW</th><th>V&gt;&gt;&gt;&gt;</th><th></th></ri<>	ESULTS R	EFLECTIN	G THE	CONSTR	RICTED FI	OW FOLLOW	V>>>>	
П	XSID:CODE SRI	E SRDL D FLEN	LEW REW	AREA K	VHD ALPH	HF HO	EGL ERR	CRWS FR#	Q VEL	WSEL
	BRDGU:BR 0.	120. 120.	6. 107.	498. 52760.	0.45 1.35	0.71 0.00	10.32 0.01	7.27 0.41	2310. 4.64	9.87
	TYPE	PPCD FLOW	v C	P/A 0.076	LSE 14.3	L BL	EN XLA ** ****	AB XRAB		
	XSID:CODE			AREA K					Q VEL	WSEL
	APP :AS 147.	120. 130.							2310. 2.23	10.53
		G) M(K)								

<><<END OF BRIDGE COMPUTATIONS>>>>

### PIER SCOUR COMPUTATIONS

FOR

Little Fork Creek at Route SC 265, Str. 134026500200, Chesterfield Co., SC Q100 Case I, No debris accumulation. Computed by NMH 10-94

	HYDRAULIC	VARIABLES	USED IN CSU EQUATION				
PIER NUMBER PIER STATION (FT) LOCATION OF PIER Y1: DEPTH (FT) V1: VEL. (FPS) a: PIER WIDTH (FT) L: PIER LENGTH (FT) PIER SHAPE ATTACK ANGLE K1 (SHAPE COEF.) K2 (ANGLE COEF.) FROUDE NO.	4 30 mcl 9.6 5.0 1.9 4.6 1 21	3 60 mcm 9.6 5.0 1.9 4.6 1 21 1.00 1.33	2 90 trb 9.6 5.0 1.9 4.6 1 21 1.00 1.33				
	COMPUTED	SCOUR DEI	THS USING CSU EQUATION				
SCOUR DEPTH (FT)	5.19	5.19	5.19				
MAX SCOUR DEPTH (FT)	571	5.71	5.71				
"MAX SCOUR DEPTH" includes an additional 10 percent of the computed CSU scour depth as recommended in HEC 18  THE COMPUTED PIER SKEW CORRECTION COEFFICIENT WAS FOUND BY EXTRAPOLATING THE LEFT END OF THE TABLE BACK TO 1 AT PIER NO. 4							
THE COMPUTED PIER SKE	W CORRECTIO	N COEFFIC	CIENT WAS FOUND				
THE COMPUTED PIER SKE	BY EXTRAPOLATING THE LEFT END OF THE TABLE BACK TO 1 AT PIER NO. 3  THE COMPUTED PIER SKEW CORRECTION COEFFICIENT WAS FOUND						
BI EXTRAPOLATING THE	LEFT END OF	THE TABL	E BACK TO 1 AT PIER NO.	2			

#### CONTRACTION SCOUR COMPUTATIONS

FOR

						-	Q1.							
Little	Fork	Creek	at Ro	oute S	SC 2	265,	Str.	13402	6500200,	Che	esterf	ield	Co.,	SC
	Q100	Case I	, No	debri	is a	accum	nulati	ion.	Computed	by	NMH	10-94		
=======================================	=====	======	====:	=====	====	====	=====	=====	=======	===	=====	=====	=====	<u> = = </u>

#### LIVE-BED SCOUR COMPUTATIONS

DISCHARGE (CFS)	MAIN CHANNEL 1380.	CONTRACTED SECTION 1320.
BOTTOM WIDTH (FT)	32.0	36.4
MANNINGS n	0.045	0.045
AVERAGE DEPTH (FT)	7.2	
ENERGY SLOPE		0.00550
D50 (FT)		0.0032
FALL VELOCITY (FPS)		0.50
K1 COEF.		0.69
K2 COEF.		0.37
COMPUTED DEPTH AT CONTRACT	ED SECTION (FT)	) = 6.3
DEPTH AT MAIN CHANNEL (FT)		= 7.2
DEPTH OF CONTRACTION SCOUR	(FT)	= -0.9

# RIGHT OVERBANK IN BRIDGE OPENING CLEAR-WATER CONTRACTION SCOUR COMPUTATIONS

DISCHARGE IN CONTRACTED SECTION (CFS)	=	393.
WIDTH OF CONTRACTED SECTION (FT)	=	44.8
MEDIAN GRAIN SIZE (FT)	=	0.0016
COMPUTED DEPTH OF CONTRACTED SECTION (FT)	=	5.2
AVERAGE FLOOD PLAIN DEPTH (FT)	=	3.3
DEPTH OF CONTRACTION SCOUR (FT)	=	1.9

#### ABUTMENT SCOUR COMPUTATIONS

FOR

Little Fork Creek at Route SC 265, Str. 134026500200, Chesterfield Co., SC Q100 Case I, No debris accumulation. Computed by NMH 10-94

# LEFT ABUTMENT SCOUR COMPUTATIONS

ABUTMENT TYPE DISCHARGE BLOCKED BY ABUTMENT (CFS) AREA BLOCKED BY ABUTMENT (SQ FT) DEPTH OF FLOW AT ABUTMENT (FT) LENGTH OF ABUT. 90 DEG. TO FLOW (FT) ABUTMENT SKEW (DEG)	3 -SPILL THROUGH 162. 188.0 3.9 134.0 21	
AJUSTED ABUTMENT LENGTH (FT) AVERAGE F/P VELOCITY U/S OF ABUT. (FPS) FROUDE NUMBER K1 COEF. K2 COEF.	48.2 0.9 0.077 0.6 1.0	
DESIGN DEPTH OF SCOUR (FROELICH EQUATION	N, 1989) (FT) = '	7.0

# RIGHT ABUTMENT SCOUR COMPUTATIONS

ABUTMENT TYPE DISCHARGE BLOCKED BY ABUTMENT (CFS) AREA BLOCKED BY ABUTMENT (SQ FT) DEPTH OF FLOW AT ABUTMENT (FT) LENGTH OF ABUT. 90 DEG. TO FLOW (FT) ABUTMENT SKEW (DEG)	3 -SPILL THROUGH 210. 258.0 0.3 169.0
AJUSTED ABUTMENT LENGTH (FT) AVERAGE F/P VELOCITY U/S OF ABUT. (FPS) FROUDE NUMBER K1 COEF. K2 COEF.	860.0 0.8 0.262 0.6 1.0

DESIGN DEPTH OF SCOUR (FROELICH EQUATION, 1989) (FT) = 5.2

### PIER SCOUR COMPUTATIONS

FOR

Little Fork Creek at Route SC 265, Str. 134026500200, Chesterfield Co., SC Q500 Case I, No debris accumulation. Computed by NMH 10-94

$\Box$					Computed by NMH	
[ ]	======================================	========		=========	==========	<b>==========</b> ==========================
		HYDRAULIC	VARIABLES	USED IN CSU	EOUATION	
					_ <b>.</b>	
	PIER NUMBER	4	3	2		
	PIER STATION (FT)	30	60	90		
	LOCATION OF PIER	mcl	mcm	trb		
L1	Y1: DEPTH (FT)	10.2	10.2	10.2		
~~	V1: VEL. (FPS)	5.9	5.9	5.9		
	a: PIER WIDTH (FT)	1.9	1.9	1.9		
[]	L: PIER LENGTH (FT)	4.6	4.6	4.6		
	PIER SHAPE	1	1	1	,	
	ATTACK ANGLE	21	21	21		
	K1 (SHAPE COEF.)	1.00	1.00	1.00		
	K2 (ANGLE COEF.)	1.33	1.33	1.33		
	FROUDE NO.	0.33	0.33	0.33		
		COMPUTED	SCOUR DEP	THS USING C	SU EQUATION	
	•					
	SCOUR DEPTH (FT)	5.62	5.62	5.62		
П						
	• • • • • • • • • • • • • • • • • • • •					
•	MAX SCOUR DEPTH (FT)	6.18	6.18	6.18		
	"MAX SCOUR DEPTH" computed CSU scour d			-	ent of the	
	THE COMPUTED PIER SKE BY EXTRAPOLATING THE					4
	THE COMPUTED PIER SKE BY EXTRAPOLATING THE					3
	THE COMPUTED PIER SKE BY EXTRAPOLATING THE					2

### CONTRACTION SCOUR COMPUTATIONS

FOR

Little Fork Creek at Route SC 265, Str. 134026500200, Chesterfield Co., SC Q500 Case I, No debris accumulation. Computed by NMH 10-94

#### LIVE-BED SCOUR COMPUTATIONS

. •	MAIN CHANNEL	CONTRACTED SECTION
DISCHARGE (CFS)	1610.	1690.
BOTTOM WIDTH (FT)	32.0	36.4
MANNINGS n	0.045	0.045
AVERAGE DEPTH (FT)	8.0	
		0.00560
EMERGI SHOFE	•	0.00560
D50 (FT)		0.0032
FALL VELOCITY (FPS)		0.50
K1 COEF.		0.69
K2 COEF.		0.37
COMPUTED DEPTH AT CONTRACT	ED SECTION (FT)	= 7.6
DEPTH AT MAIN CHANNEL (FT)		= 8.0
DEPTH OF CONTRACTION SCOUR	(FT)	= -0.4

# RIGHT OVERBANK IN BRIDGE OPENING CLEAR-WATER CONTRACTION SCOUR COMPUTATIONS

DISCHARGE IN CONTRACTED SECTION (CFS)	=	577.
WIDTH OF CONTRACTED SECTION (FT)	=	44.8
MEDIAN GRAIN SIZE (FT)	=	0.0016
COMPUTED DEPTH OF CONTRACTED SECTION (FT)	=	7.2
AVERAGE FLOOD PLAIN DEPTH (FT)	=	3.9
DEPTH OF CONTRACTION SCOUR (FT)	=	3.3

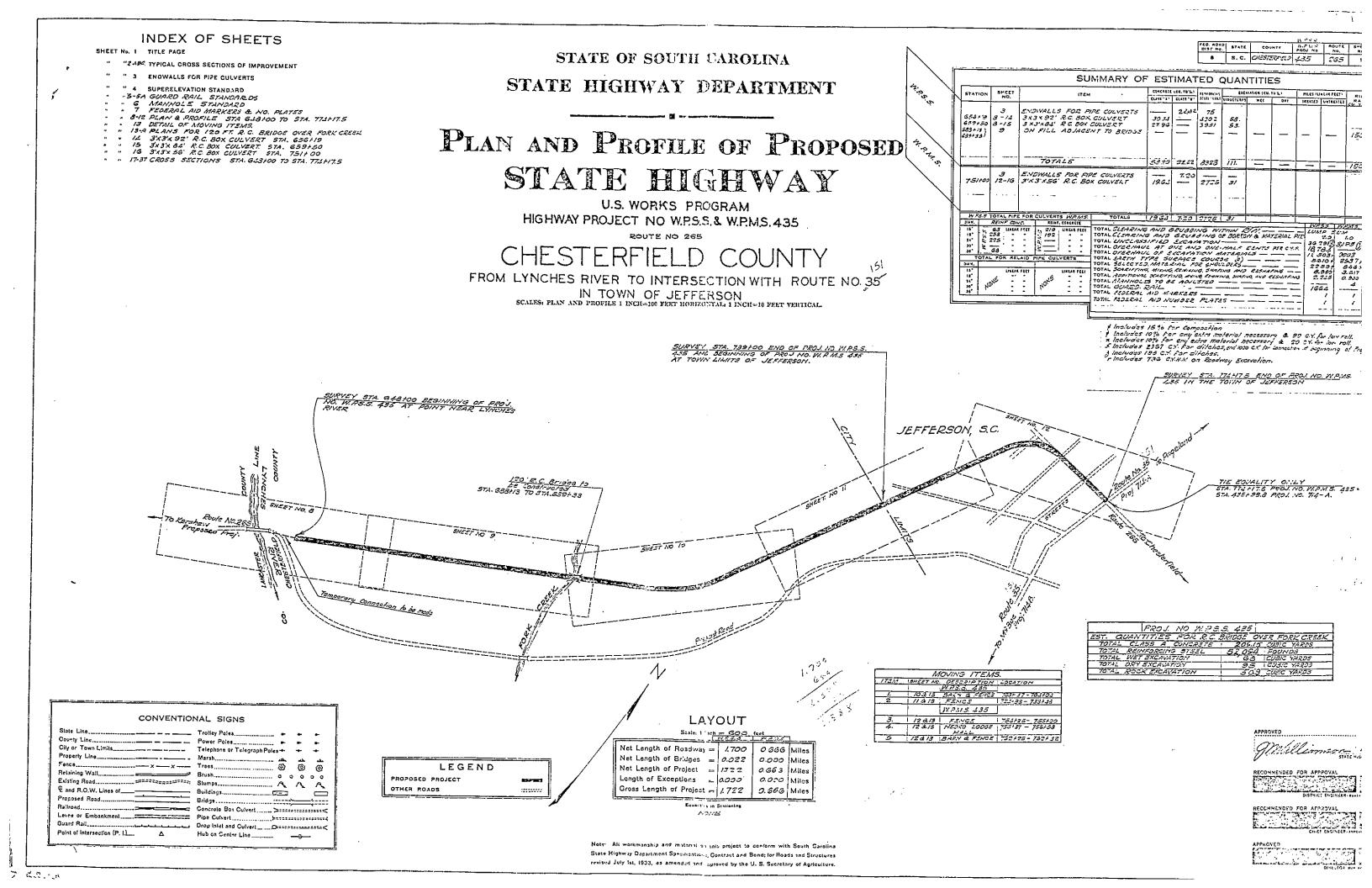
### ABUTMENT SCOUR COMPUTATIONS

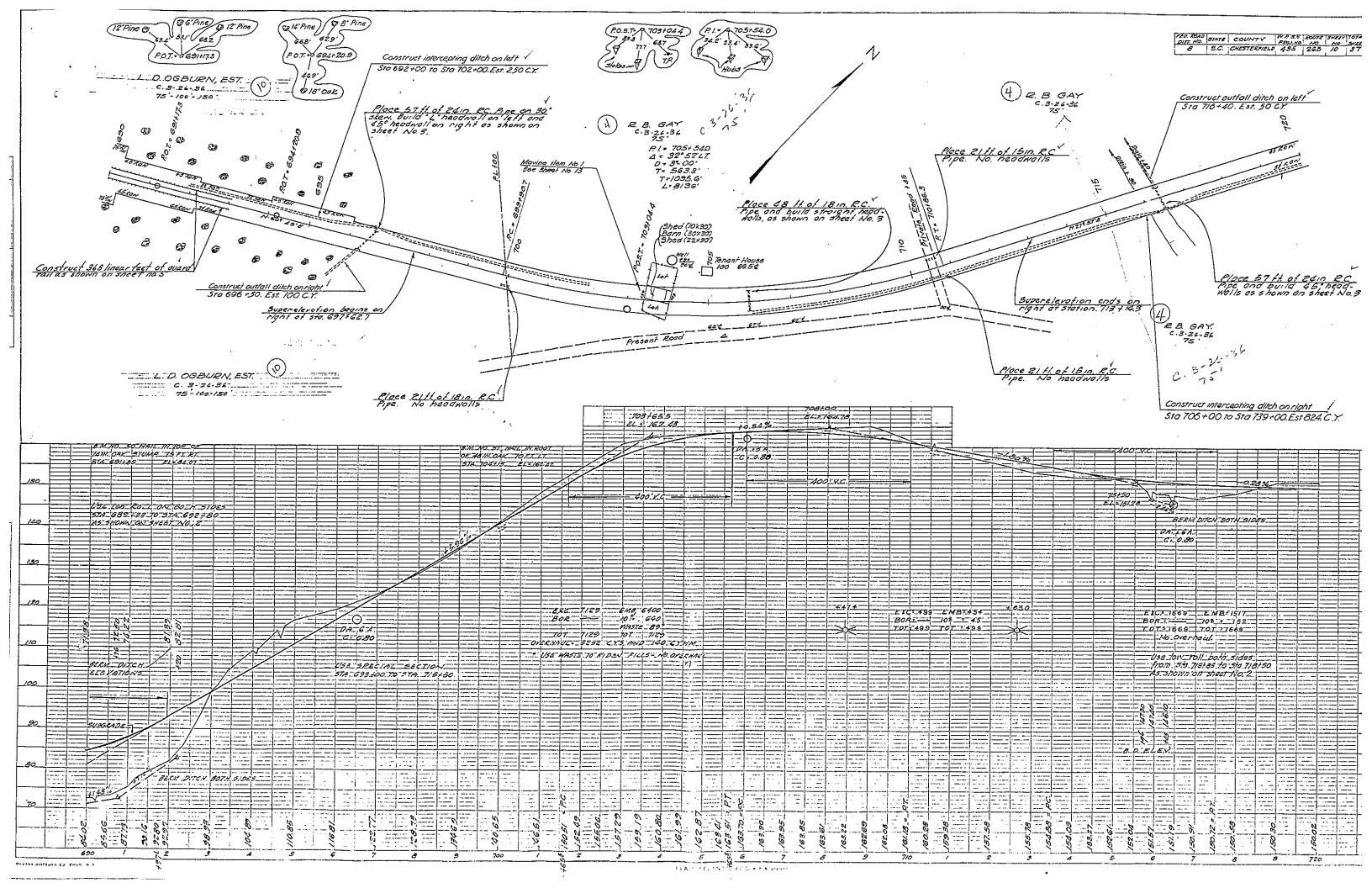
FOR

Little Fork Creek at Route SC 265, Str. 134026500200, Chesterfield Co., SC Q500 Case I, No debris accumulation. Computed by NMH 10-94

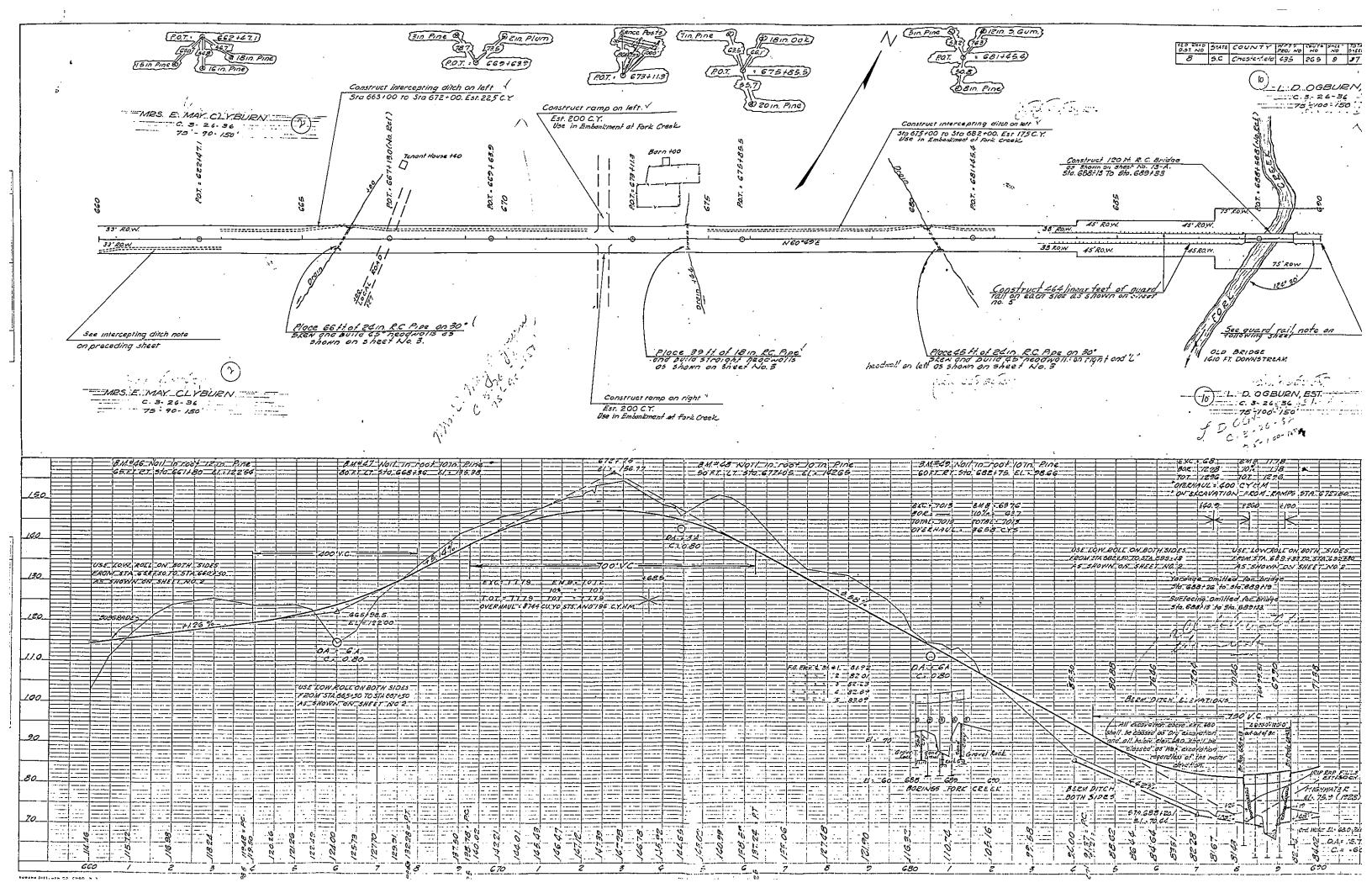
	·	EFT ABUTMENT	
	SCOU	R COMPUTATIONS	
	ABUTMENT TYPE DISCHARGE BLOCKED BY ABUTMENT (CFS) AREA BLOCKED BY ABUTMENT (SQ FT)	3 -SPILL THROUGH 225. 297.0	
	DEPTH OF FLOW AT ABUTMENT (FT) LENGTH OF ABUT. 90 DEG. TO FLOW (FT) ABUTMENT SKEW (DEG)	4.5 153.0 21	
	AJUSTED ABUTMENT LENGTH (FT) AVERAGE F/P VELOCITY U/S OF ABUT. (FPS) FROUDE NUMBER	66.0 0.8 0.063	
	K1 COEF. K2 COEF.	0.6 1.0	
	DESIGN DEPTH OF SCOUR (FROELICH EQUATION	N, 1989) (FT) =	7.9
		GHT ABUTMENT R COMPUTATIONS	
	ABUTMENT TYPE DISCHARGE BLOCKED BY ABUTMENT (CFS) AREA BLOCKED BY ABUTMENT (SQ FT)	3 -SPILL THROUGH 406. 425.0	
	DEPTH OF FLOW AT ABUTMENT (FT) LENGTH OF ABUT. 90 DEG. TO FLOW (FT) ABUTMENT SKEW (DEG)	0.9 200.0 -21	
	AJUSTED ABUTMENT LENGTH (FT) AVERAGE F/P VELOCITY U/S OF ABUT. (FPS) FROUDE NUMBER	472.2 1.0 0.177	
	K1 COEF. K2 COEF.	0.6 1.0	
ra			

DESIGN DEPTH OF SCOUR (FROELICH EQUATION, 1989) (FT) = 6.5





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## United States Department of the Interior



GEOLOGICAL SURVEY
Water Resources Division
Stephenson Center, Suite 129
720 Gracern Road
Columbia, SC 29210-7651

October 17, 1994

William H. Hulbert, P.E. Hydraulic Engineer South Carolina Department of Transportation 955 Park Street Columbia, South Carolina 29202

Dear Mr. Hulbert:

We are pleased to transmit to you another report of the Level II Bridge Scour Program titled, "Level II bridge scour analysis for structure 134026500200 on Route SC 265, crossing Little Fork Creek in Chesterfield County, South Carolina," by Noel M. Hurley, Jr. and Stephen T. Benedict. This report has been reviewed and approved by the U.S. Geological Survey, S.C. District.

If you have any questions concerning this report please contact me (750-6126) or Stephen Benedict (750-6150) and we will be glad to assist you.

Sincerely

Noel M. Hurley, Jr.

Supervisory Hydrologist/

Enclosure



